



## On the selectivity of cobalt-based Fischer–Tropsch catalysts: Evidence for a common precursor for methane and long-chain hydrocarbons

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### ABSTRACT

A total of 36 cobalt-based supported catalysts were investigated in the Fischer–Tropsch reaction at industrially relevant process conditions: 483 K, 20 bar, molar H<sub>2</sub>/CO ratio = 2.1, pellet size: 53–90 μm. The effect of adding water vapour to the feed was investigated for 20 of the catalysts, and a H<sub>2</sub>/CO ratio of 1.0 was used for a few catalysts. The catalysts differed in support material, Co loading, promoters, Cl content, Co particle size (larger than ~6 nm), morphology, degree of reduction and preparation technique and showed a large variation in selectivity. For each set of process conditions, a linear relationship seems to exist between the selectivity to methane (and other light products) and C<sub>5+</sub>, indicating a common precursor, i.e. a common monomer pool, for all hydrocarbon products. A high selectivity to C<sub>5+</sub> is mainly an effect of a high intrinsic chain-growth probability and unlikely to be a result of an enhanced  $\alpha$ -olefin readsorption. The universal effect of external water addition on the hydrocarbon selectivities is limited to a decrease in the methane selectivity. A small proportion of the catalysts developed “pure methanation” sites upon exposure to high partial pressures of water.

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### 1. Introduction

In the Fischer–Tropsch (FT) synthesis, hydrocarbons (HCs) are produced from synthesis gas (H<sub>2</sub> + CO) at elevated pressure, typically over a cobalt- or iron-based catalyst. Due to the FT mechanism of stepwise chain growth, the highest yield to FT diesel is achieved by first making waxes, i.e. very long hydrocarbon chains, and then hydrocracking these into the diesel fraction (~C<sub>12</sub>–C<sub>18</sub>). In this way, the production of lighter by-products is minimised. The typical FT-product distribution with respect to carbon number is called the Anderson–Schulz–Flory (ASF) distribution, in which the chain-growth probability ( $\alpha$  value) is assumed to be constant and therefore independent of chain length. The ability of a catalyst to produce higher hydrocarbons is often indicated by the  $\alpha$  value or by the industrially relevant parameter S<sub>C<sub>5+</sub></sub> (selectivity to C<sub>5</sub> and higher hydrocarbons). Naturally, a higher S<sub>C<sub>5+</sub></sub> results in a more efficient conversion from synthesis gas to diesel fuel.

Provided that the synthesis gas has the correct H<sub>2</sub>/CO ratio (approx. 2), supported cobalt catalysts are preferred in the FT process when waxes are the desired product, due to the reasonable price of

the metal, high activity and high selectivity to higher hydrocarbons and low water–gas shift activity. For the obtained product distributions over Co-based catalysts, there are always some deviations from the ASF model. For instance, two different  $\alpha$  values are often used to describe the product distribution: one lower ( $\alpha_1$ ) for carbon numbers between ~5 and ~10–20 and one higher ( $\alpha_\infty$ ) for higher carbon numbers [1,2]. Furthermore, the selectivity to methane (S<sub>C<sub>1</sub></sub>) is always significantly higher and that to C<sub>2</sub> (S<sub>C<sub>2</sub></sub>) significantly lower than predicted by the ASF model [3], while for standard alkali-Fe-based catalysts, the C<sub>1</sub> and C<sub>2</sub> fractions are not deviating significantly from an ASF distribution [4–6]. The main products from the Co-catalysed FT synthesis are linear paraffins and olefins. The  $\alpha$ -olefins may readsorb on the catalyst and react further to produce longer HCs (reinsertion or initiation) or they may be hydrogenated to form the corresponding paraffins.

Several reasons have been proposed for the higher  $\alpha$  value for higher HCs. It could be the result of a higher degree of  $\alpha$ -olefin readsorption (due to chain-length-dependent diffusion rate, solubility in wax and/or physisorption) followed by further chain growth [1,2,7,8] or two different chain-growth mechanisms with different monomers on one [9,10] or two [11] type/s of active site/s. The occurrence of different catalytic sites with different chain-growth probabilities [12] and two different termination

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pathways occurring on the same type of site [13] has also been proposed. However, constant  $\alpha$  values for the  $C_{5+}$  fraction for a number of Co-based catalysts under different process conditions have also been reported [14], as well as a smoother increase in  $\alpha$  value with carbon number ascribed to a successive increase in the true propagation probability with carbon number [15]. Some of the observed deviations from ASF have been questioned and attributed to artefacts associated with product analyses [14–16]. The high  $S_{C_1}$  has been explained by an increased surface mobility of the methane precursor [13] and by different reaction mechanisms and/or active sites for methanation (dissociation of CO) and chain growth (CO insertion) [6,17,18]. The low selectivity to  $C_2$  has been explained by a much higher readsorption rate constant for ethene compared to higher  $\alpha$ -olefins [1,14].

The differences in  $S_{C_{5+}}$  for Co-based catalysts have been attributed to different extents of  $\alpha$ -olefin readsorption (followed by further chain growth) [2], the extent of  $\alpha$ -olefin readsorption in turn being governed by the degree of mass transfer restrictions on the product removal (i.e. pore size, catalyst pellet size, active site density and porosity). The importance of secondary reactions on the  $S_{C_{5+}}$  has, however, recently been questioned [19–21] and Co particle size effects [20,22,23], as well as effects of the support material [20], on the intrinsic chain-growth probability and, accordingly, on the  $S_{C_{5+}}$  have been presented. The observed increase in olefin/paraffin (o/p) ratio, for a certain carbon number, with  $S_{C_{5+}}$  was interpreted as if the contribution of  $\alpha$ -olefin readsorption to an increased  $S_{C_{5+}}$  could only be of minor importance [20]. Recently, it was reported that for Co supported on carbon nanofibres, i.e. a possible inert support material, the  $S_{C_{5+}}$  increases with Co particle size up to 6 nm, after which it levels out [23]. This was found to be due to a decreasing surface coverage of hydrogen with increasing Co particle size up to 6 nm. Differences in surface coverages have also been suggested to govern the  $S_{C_{5+}}$  for catalysts with Co particles larger than 6 nm [24,25].

Proposed reasons for the well-documented increase in  $S_{C_{5+}}$  upon a lowered space velocity (increased conversion) include increased  $\alpha$ -olefin readsorption due to the longer bed residence time [1,5] and increased partial pressure of water [21,26,27]. The promoting effect of water on the  $S_{C_{5+}}$  has been proposed to be due to its inhibition of hydrogenation reactions, by competitive adsorption, yielding lower methane selectivity and higher probability of olefin readsorption and further growth [18,28,29], as well as due to an increased surface coverage of the active surface carbon (i.e. the monomer pool) [30].

Although relatively mature, there are obviously still uncertainties regarding some fundamental aspects of the Co-catalysed FT synthesis process, in particular the parameters governing the product selectivity of catalysts with Co particles larger than approximately 6 nm on different support materials (under conditions where mass transfer limitations on reactants arrival are absent). In the present paper, selectivity results from careful experimental studies of a range of Co-based catalysts are presented and discussed with focus on evaluating the possible importance of secondary reactions and separate methanation sites on the  $S_{C_{5+}}$ . Discussing in detail what characteristics give a catalyst high  $S_{C_{5+}}$  is outside the scope of the present paper.

## 2. Experimental

### 2.1. Preparation of catalysts

A total of 36 Co-based supported catalysts were prepared. Two different preparation techniques were used: incipient wetness impregnation (IW) and microemulsion (ME). The catalysts were prepared on three different support materials ( $\gamma$ - $Al_2O_3$ ,  $\alpha$ - $Al_2O_3$  and  $TiO_2$ ), with varying Co loadings (4–30 wt%), promoters (Re (0

or 0.5 wt%) or B (0–0.15 wt%). In addition, two IW- $\gamma$ - $Al_2O_3$  catalysts contained residues of Cl, as they were prepared from  $CoCl_2$ . Furthermore, three catalysts were exposed to hydrothermal treatment (HT) after being prepared by the IW or ME techniques, and one IW-prepared catalyst was additionally reduced and oxidised (RedOx). It should be mentioned that the ME-prepared catalysts contained residues of B from the preparation (0.03 wt% for the ME- $\alpha$ - $Al_2O_3$  and 0.15–0.18 wt% for ME- $\gamma$ - $Al_2O_3$  and ME- $TiO_2$ ), while essentially all Cl from the preparation of these ME catalysts was removed in the wash (<0.02 wt% left).

The  $\gamma$ - $Al_2O_3$  (Puralox SCCA-5/200 from Sasol) and  $TiO_2$  (Degussa P25) support materials were dried at 393 K for 6 h and then calcined in flowing air for 10 h at 773 K and 973 K (ramp = 1 K/min), respectively. The  $\alpha$ - $Al_2O_3$  support was prepared from the  $\gamma$ - $Al_2O_3$  support by calcining it in flowing air at 1373 K for 10 h. For both the  $TiO_2$  and  $\alpha$ - $Al_2O_3$  support materials, actually three different batches were used that differed slightly in physical properties.

For the IW preparations, the support materials were impregnated with aqueous solutions of  $Co(NO_3)_2 \cdot 6H_2O$  (ACS reagent,  $\geq 99.0\%$ , Fluka) and, in some cases,  $HReO_4$  (Alfa Aesar) or  $B_2O_3$  ( $\geq 98.0\%$ , Fluka). In two cases, an aqueous solution of  $CoCl_2 \cdot 6H_2O$  (99.9% (metals basis), Alfa Aesar) was used instead of cobalt nitrate. Three impregnations, with intermediate drying at 373 K for 1 h, were used. The powder was then dried at 393 K for 3 h and calcined in air at 573 K for 16 h (ramp = 1 K/min) in a crucible standing in the oven. One of the IW catalysts prepared from  $CoCl_2$  was, however, calcined at 773 K as  $CoCl_2$  was found not to decompose at the lower temperature. The Cl contents of the IW catalysts prepared from  $CoCl_2$ , prior to reduction, were 7.7 wt% (calcined at 573 K) and 1.5 wt% (calcined at 773 K), respectively.

For the ME preparations, the following components were mixed in order to form the microemulsion:

*Oil phase (69.8 wt%):* cyclohexane (ACS reagent,  $\geq 99.0\%$ , Sigma Aldrich)

*Surfactant (19.9 wt%):* Berol 02, polyoxyethylene (6) nonylphenyl ether (Akzo Nobel)

*Water phase (10.3 wt%):* aqueous solution of  $CoCl_2 \cdot 6H_2O$  (99.9% (metals basis), Alfa Aesar) and  $HReO_4$  (Alfa Aesar). [ $Co^{2+}$ ] in water phase: 0.12 M. [ $Re^{7+}$ ] in water phase: 1.6 mM.

In order to form a sol (i.e. solid Co-containing particles dispersed in the oil phase) from the microemulsion, a  $NaBH_4$  (98% min, Alfa Aesar) aqueous solution (10 M) was added as a reducing agent. A molar ratio of  $BH_4^-/Co^{2+}$  of 3 was used. The reduction step was performed in a  $N_2$  atmosphere in a glove bag. The Co-containing particles were deposited onto the supports by destabilisation of the organosol with acetone (50 cm<sup>3</sup> acetone/100 g sol) in the presence of the support under vigorous stirring for 2–3 h. In total, for  $\gamma$ - $Al_2O_3$  and  $TiO_2$ , six depositions were made in which approximately 2 wt% of Co (and 0.083 (=0.5/6) wt% Re) was added to the support in each deposition to finally reach a Co loading of 12 wt%. For  $\alpha$ - $Al_2O_3$ , a Co loading not higher than 4.4 wt% was achieved after 10 depositions, as only a small proportion of the Co particles were attached to the support. After each deposition, the catalyst powders were washed with ethanol, acetone and water at room temperature and then dried at 323 K overnight. After the last deposition, the water for the wash had a temperature of 373 K. After the final deposition and wash, the ME catalysts were dried for at least 16 h at 323 K and then calcined in air at 573 K for 16 h (ramp = 1 K/min). The majority of the added Re was found to be removed in the wash.

In the hydrothermal treatment mentioned above, three catalysts were exposed to water vapour at 873 K in flowing air for 5 h. The one catalyst exposed to the RedOx treatment mentioned above was, after being prepared according to the IW procedure,

first reduced in hydrogen at 623 K for 16 h, then passivated (in N<sub>2</sub> 5.0 for 0.5 h and in 0.5 vol% O<sub>2</sub> in N<sub>2</sub> for 1 h at room temperature) and finally calcined again in air at 573 K for 16 h.

## 2.2. Catalyst characterisation techniques

Brunauer–Emmett–Teller (BET) surface area and porosity measurements for the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-supported catalysts were performed in a Micromeritics ASAP 2000/2010 unit. The samples were evacuated and dried at 523 K overnight prior to analysis. The BET area was estimated by N<sub>2</sub> adsorption at liquid nitrogen temperature at relative pressures between 0.06 and 0.2. The total pore volume was estimated from a single point of adsorption at  $p/p^0 = 0.998$ , and the average pore diameter was estimated from the pore volume and BET surface area assuming cylindrical pores. Internal surface area and porosity measurements for the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub>-supported catalysts were performed in a Micromeritics Mercury Porosimeter, AutoPore IV.

Oxygen titration was performed in order to estimate the degree of reduction (DOR) of the catalysts after reduction under flowing hydrogen for 16 h at the reduction temperature used prior to FT experiments (623 or 673 K) and has been described elsewhere [31,32]. The DOR was calculated assuming that all cobalt in metallic form was oxidised to Co<sub>3</sub>O<sub>4</sub>.

The DOR was also estimated from temperature programmed reduction (TPR) of the reduced samples: after reduction in flowing hydrogen for 16 h at 623/673 K, the samples were purged with helium for 1 h at the reduction temperature, then brought down to room temperature in flowing helium and finally TPR was performed. The catalyst samples were heated at a rate of 10 K/min to 1203 K in a flow of 7% H<sub>2</sub> in argon. The hydrogen consumption was measured by comparing the thermal conductivity of the inlet and outlet gas. Calibration was done by the reduction of Ag<sub>2</sub>O powder. The DOR was calculated assuming that the unreduced cobalt in the reduced catalysts (after 16 h at 623/673 K) was composed of Co(II) as evidenced from X-ray absorption spectroscopy [33].

The procedure of measuring H<sub>2</sub> adsorption isotherms of the catalysts, in order to estimate the Co dispersion ( $D$ , %), has been described elsewhere [31,32]. Briefly, the measurements were conducted on a Micromeritics ASAP 2010 unit at 313 K, after reducing the calcined catalysts in flowing hydrogen at 623/673 K for 16 h. Since the chemical adsorption of H<sub>2</sub> on Co has been reported to be reversible [34] and since physical adsorption of H<sub>2</sub> on Co is negligible [35], the adsorption data from a single isotherm were used for dispersion estimates. It was assumed that the adsorption stoichiometry is 1 H<sub>2</sub> on 2 Co (or H:Co = 1) [36] and that Re does not contribute to the amount of hydrogen adsorbed. The particle size ( $d$ , nm) of Co<sup>0</sup> is estimated according to the following equation [20,37]:

$$d = \frac{96}{D} \cdot \text{DOR} \quad (1)$$

Reduced (in hydrogen at 623/673 K for 16 h) and passivated (in N<sub>2</sub> 5.0 for 0.5 h and in 0.5 vol% O<sub>2</sub> in N<sub>2</sub> for 1 h at room temperature) catalysts were prepared for transmission electron microscopy (TEM) by ultramicrotomy after first embedding in an organic resin. TEM analysis was performed using a JEOL 2010F instrument operating at 200 kV equipped with an Oxford Instruments X-ray detector for energy dispersive spectroscopy (EDS) composition analysis. Conventional TEM was performed under bright-field diffraction contrast conditions. For EDS, the microscope was operated in scanning transmission electron microscopy (STEM) mode with a nominal probe diameter of ~0.7 nm. STEM images were acquired using an annular dark field detector, which provides contrast that has a strong dependence on atomic number.

X-ray diffraction (XRD) was performed on the calcined and/or reduced and passivated samples using a Siemens D5005 X-ray diffractometer with Cu K $\alpha$  radiation. A secondary monochromator was used. Crystallite thicknesses of Co<sub>3</sub>O<sub>4</sub> and/or Co were estimated by using the Scherrer formula [35]. Assuming spherical crystallites, the diameter of the particles was estimated by correcting the crystallite thickness by a factor 4/3 [35]. When the Co crystallite size was estimated from that of Co<sub>3</sub>O<sub>4</sub>, the following formula was used [38]:

$$d(\text{Co}^0) = 0.75 \cdot d(\text{Co}_3\text{O}_4) \quad (2)$$

according to the relative molar volumes of metallic cobalt and Co<sub>3</sub>O<sub>4</sub>.

## 2.3. Fischer–Tropsch experiments

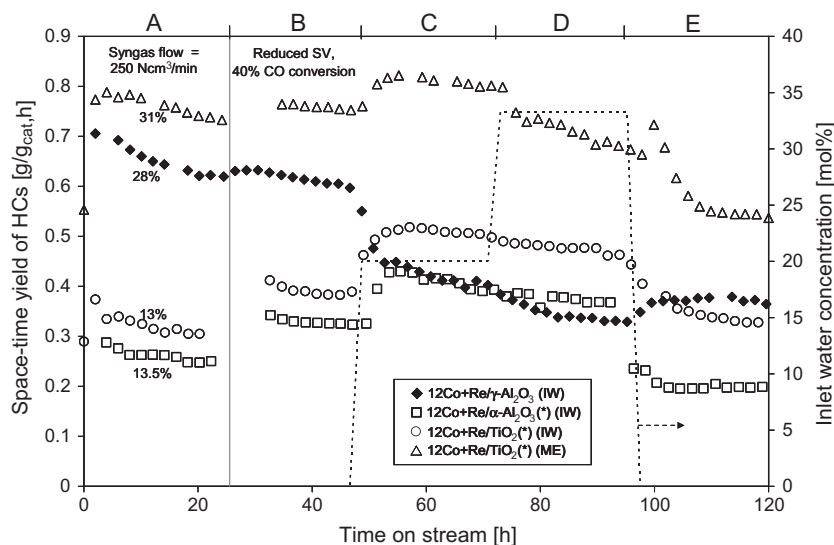
A detailed description of the equipment and procedure has been given elsewhere [19,32]. Briefly, FT synthesis was performed in a stainless-steel fixed-bed reactor (i.d. 10 mm) at the following reference case process conditions: 483 K, 20 bar, molar H<sub>2</sub>/CO ratio = 2.1, catalyst pellet size: 53–90  $\mu\text{m}$ . The catalysts were diluted with SiC to achieve an even temperature profile and reduced *in situ* in hydrogen for 16 h at atmospheric pressure prior to the FT experiments, at 623 K and 673 K for IW and ME-prepared catalysts, respectively, as the ME catalysts had significantly lower reducibilities. Also, the two Cl-containing IW catalysts were reduced at 673 K.

Initial reactant flow (period A) was 250 N cm<sup>3</sup>/min (or gas hourly space velocity 5000–15,000 N cm<sup>3</sup>/g<sub>cat</sub>, h depending on amount of catalyst) and held for approximately 24 h. Then, the space velocity was lowered to achieve approximately 40% CO conversion (period B) and held for another 24 h. A total of 20 of the catalysts were held further on stream and exposed to different amounts of water vapour in the feed the following 48 h (20% in period C and 33% in period D). Water vapour was introduced by passing deionised water through an electrical vaporiser kept at 623 K and mixed with the synthesis gas prior to the reactor inlet. The total pressure and flow of synthesis gas were kept constant during external water addition, which implies that the partial pressures of the reactants were lower in periods C and D. In the last period (E) for these 20 catalysts, the water feed was shut off, and the experimental conditions were the same as in period B. The different periods (A–E) are illustrated in Figs. 1 and 2. A small proportion of the catalysts were also tested under a molar H<sub>2</sub>/CO ratio of 1.0.

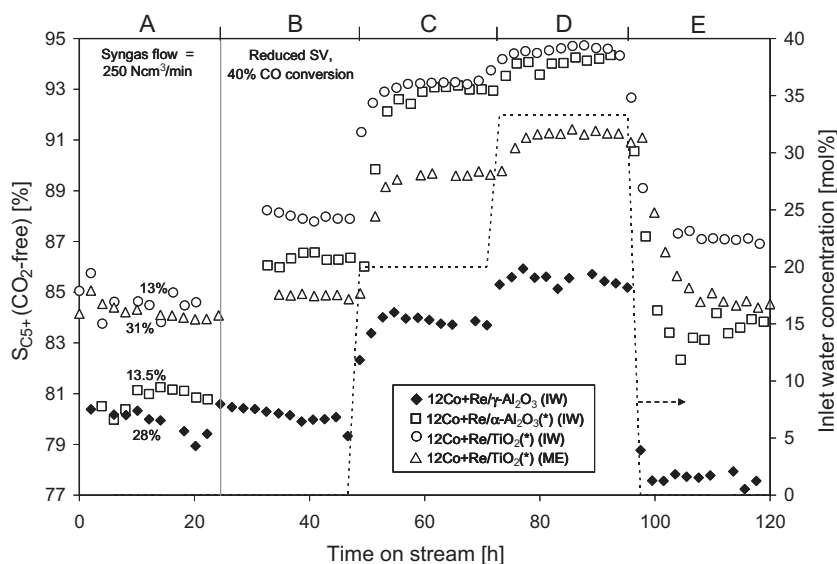
The heavy HCs and most of the liquid products were collected in a heated trap (363 K). The product gases also passed through a “cold” trap at room temperature in order to condense residual liquid products, before gas analysis. The product gases (C<sub>1</sub>–C<sub>6</sub> HCs and CO<sub>2</sub>), as well as N<sub>2</sub> and unconverted CO, were analysed on line by a HP 5890 gas chromatograph equipped with a thermal conductivity detector (TCD) and a flame ionisation detector (FID). N<sub>2</sub> was used as an internal standard. Quantitative analyses of C<sub>1</sub>–C<sub>4</sub> HCs were performed and allowed for SC<sub>5+</sub> determination. The SC<sub>5+</sub> is defined as follows (after correction for the low SC<sub>CO<sub>2</sub></sub> (<2% in dry periods)):

$$SC_{5+} = 100 - (SC_1 + SC_2 + SC_3 + SC_4) \quad (3)$$

Quantitative analyses of C<sub>5</sub> and C<sub>6</sub> HCs existing in the gas phase were also made. By assuming gas/liquid equilibrium in the cold trap (calculated by using Aspen HYSYS 2006, equation of state: Lee Kesler Plocker, 298 K, 20 bar), the total amount of C<sub>5</sub> and C<sub>6</sub> HCs could be estimated from the gas analysis. Formation of oxygenates over these Co-based catalysts has been assumed negligible. All reported selectivities are C-atom based and CO<sub>2</sub>-free.



**Fig. 1.** Space-time yields of hydrocarbons for three IW catalysts (12 wt% Co, 0.5 wt% Re) and the ME-TiO<sub>2</sub> catalyst during 5 days on stream. The %-numbers in the first period indicate the CO conversions in the middle of period A. After 24 h on stream, the space velocity (SV) (and accordingly the synthesis gas flow) was lowered so as to reach a CO conversion of 40% (period B). The same synthesis gas flow was used during periods C, D and E. Water vapour was added to the feed, in different amounts, during the third and fourth day (C and D). Reaction conditions: 483 K,  $P_{\text{tot}} = 20$  bar,  $\text{H}_2/\text{CO} = 2.1$  (the synthesis gas pressure was reduced upon water introduction since no correction with inert gas was made).



**Fig. 2.**  $S_{\text{C}_5^+}$  vs. time on stream for the catalysts shown in Fig. 1.

### 3. Results

#### 3.1. Characterisation of catalysts

Table 1 shows the physical properties of the pure support materials and of some selected catalysts. The  $\gamma\text{-Al}_2\text{O}_3$  is a typical narrow-pore support with high surface area, while  $\alpha\text{-Al}_2\text{O}_3$  and  $\text{TiO}_2$  have larger pores and lower surface areas. The  $\alpha\text{-Al}_2\text{O}_3$  was prepared by heat treatment of the  $\gamma\text{-Al}_2\text{O}_3$ , as mentioned in Section 2.1.

Table 2 shows the physicochemical properties of all studied catalysts. The number in front of the element (Co or B) indicates the loading in wt%. For all Re-promoted catalysts, the nominal loading was 0.5 wt% Re but, as mentioned in Section 2.1, the Re content in the ME catalysts was significantly lower. The DOR (degree of reduction) of the catalysts, as measured by oxygen titration, varied be-

tween 22% and 71%. The DOR estimated from TPR measurements were significantly higher and, probably, more correct as reported earlier [19]. Hence, this DOR was used together with dispersion measurements for cobalt particle size estimations (according to Eq. (1) above), which ranged between 6 and 42 nm. All catalysts, except for the ME- $\gamma\text{-Al}_2\text{O}_3$  catalyst, had crystalline Co particles, as evidenced from XRD.

When using the IW technique, the large-pore supports ( $\alpha\text{-Al}_2\text{O}_3$  and  $\text{TiO}_2$ ) resulted in larger Co particles than the narrow-pore  $\gamma\text{-Al}_2\text{O}_3$ , which is a well-known phenomenon [19,32,39]. When using the ME technique with  $\alpha\text{-Al}_2\text{O}_3$  and  $\text{TiO}_2$ , the resulting Co particle sizes were similar to that of the IW- $\gamma\text{-Al}_2\text{O}_3$  catalysts (prepared from  $\text{Co}(\text{NO}_3)_2$ ) and approximately half of the size in the corresponding IW catalysts (for the same batch of support material). Increasing the Co loading in the IW preparations generally increased both the  $\text{Co}_3\text{O}_4$  crystallite size in the calcined catalysts



**Table 1**

Physical properties of the pure support materials and of some selected catalysts. IW, incipient wetness impregnation; ME, microemulsion.

Catalyst	Average pore diameter <sup>a</sup> (nm)	Surface area (A) (m <sup>2</sup> /g <sub>cat</sub> )	Pore volume (V) (cm <sup>3</sup> /g <sub>cat</sub> )
$\gamma$ -Al <sub>2</sub> O <sub>3</sub>	10.4	193	0.5
6Co (IW)	9.6	181	0.44
12Co (IW)	9.3	173	0.40
12Co + Re (IW)	8.9	172	0.38
20Co (IW)	8.5	148	0.31
12Co + Re (ME)	10.2	201	0.51
$\alpha$ -Al <sub>2</sub> O <sub>3</sub>	72	11.7	0.21
6Co (IW)	66	10.4	0.17
12Co (IW)	62	10.4	0.16
20Co (IW)	50	10.4	0.13
$\alpha$ -Al <sub>2</sub> O <sub>3</sub> (*)	65	11.1	0.18
12Co + Re (IW)	58	8.3	0.12
4.4Co + Re (ME)	57	11.3	0.16
TiO <sub>2</sub>	193	26.1	1.26
6Co (IW)	106	17.4	0.46
12Co (IW)	90	15.5	0.35
20Co (IW)	111	13.7	0.38
30Co (IW)	91	12.7	0.29
TiO <sub>2</sub> (*)	257	23.2	1.49
12Co + Re (IW)	273	13.2	0.90
12Co + Re (ME)	174	20.2	0.88

<sup>a</sup> The average pore diameter ( $d_p$ ) estimated from surface area (A) and pore volume (V) according to:  $d_p = \frac{4V}{A}$ .

and the Co particle size in the reduced catalysts. The Co loading, as well as Re promotion, had a strong influence on the DOR of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-supported catalysts, while a much less pronounced effect was found for the other catalysts. This may be ascribed to Co(II) ions entering some of the tetrahedral vacancies of the defect spinel structure of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> upon reduction [40]. Re inhibits the formation of these hard-to-reduce Co-support species and also facilitates the reduction of CoO interacting strongly with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [41]. As seen from Table 2, there was no unequivocal effect on the Co particle size of the addition of 0.5 wt% Re to the 12 wt% Co catalysts. The addition of 0.15 wt% B, however, seemingly reduced the Co<sub>3</sub>O<sub>4</sub> crystallite size, as reported earlier [42], while the effect on the Co particle size is unclear. Addition of B clearly decreased the DOR [42].

The dispersion measurements on the two Cl-containing IW catalysts largely overestimated the Co particle sizes, probably due to residual Cl being adsorbed onto the Co sites. Hence, XRD of the reduced and passivated samples was used for particle size estimation instead. By using CoCl<sub>2</sub> instead of the nitrate, significantly larger Co particles were formed on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>; 25 and 16 nm for the CoCl<sub>2</sub>-based catalysts calcined at 573 K and 773 K, respectively, compared to 9 nm for the corresponding Co(NO<sub>3</sub>)<sub>2</sub>-based catalyst calcined at 573 K (as measured from XRD of reduced and passivated samples, see Table 2). The morphologies of the Cl-containing IW catalysts were also found to be very different. Fig. 3a illustrates the Co distribution in the IW- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst prepared from Co(NO<sub>3</sub>)<sub>2</sub> where Co particles form aggregates within the support pore structure [43]. Fig. 3b illustrates the Co distribution in the IW- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst prepared from CoCl<sub>2</sub>, in which no Co particle aggregates were found. Of course, not only the choice of Co precursor but also the choice of support material greatly affects the structure of the final catalyst. For example, similar well-defined aggregates of Co particles as illustrated in Fig. 3a were not found in the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> or TiO<sub>2</sub>-supported catalysts, as seen from Fig. 3c and d, respectively.

The ME technique also yielded a different distribution of the Co particles over the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> supports compared to the

IW technique. The strongest effect was seen for the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-supported catalyst. Fig. 3e shows that for the ME sample, the small pores of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> resulted in deposition of a significant proportion of the Co particles on the external surface of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> pellets, suggesting that the Co particles surrounded by surfactant molecules were generally too big to enter the pores of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> during destabilisation of the sol. This distribution was confirmed by EDS X-ray analysis and mapping, where a strong Co signal was obtained from the irregular material indicated by arrows, while a comparatively weak Co signal was obtained from within the pellets. As mentioned above, the Co phase of the fresh ME- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was XRD amorphous.

The hydrothermal treatment, which was performed with three of the catalysts, increased the Co particle size of the ME- $\alpha$ -Al<sub>2</sub>O<sub>3</sub> catalyst (from 11 to 17 nm, estimated from XRD of calcined catalysts), while the Co particle sizes appeared rather unchanged for the IW- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and IW- $\alpha$ -Al<sub>2</sub>O<sub>3</sub> catalysts, as seen in Table 2. The IW- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, however, lost a significant part of its FT activity and selectivity to higher HCs, probably due to the formation of inactive Co–Al species during the hydrothermal treatment, as indicated from XRD measurements and from a lowered degree of reduction.

Assuming an unchanged site activity, the RedOx treatment of the IW-TiO<sub>2</sub> catalyst reduced the Co particle size with 25%.

### 3.2. Activity results

It has been shown that for catalysts with Co particle sizes above approximately 6 nm, the site activity, or turnover frequency (TOF), is relatively constant at constant process conditions [22,23,28,32,44,45] and hence independent of support material and HC selectivities. This is also the case for the majority of the catalysts in the present study (see Table 2), for which the site activity (mol CO converted/mol surface Co, s) after 10 h on stream under reference case process conditions varied mainly between 0.044 and 0.08 s<sup>-1</sup>. Some of the TiO<sub>2</sub>-supported catalysts had higher site activities, but this is probably due to an underestimation of the dispersion due to TiO<sub>x</sub> decoration [36].

In Fig. 1, the space-time yields to hydrocarbons vs. time on stream are shown for four selected catalysts with the same nominal loadings (12 wt% Co, 0.5 wt% Re). The higher productivity of the ME-TiO<sub>2</sub>(\*) catalyst, when compared to its IW counterpart, is a result of the smaller Co particles obtained when using the ME technique. The large-pore-supported catalysts tended to react positively to the external water addition, while the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-supported catalysts generally lowered their FT rates.

### 3.3. Selectivity results

In Fig. 2, the S<sub>C<sub>5+</sub></sub> vs. time on stream are shown for the same catalysts as shown in Fig. 1. In the following subparagraphs, the selectivities under the reference case process conditions (i.e. periods A and B), as well as under changed conditions (e.g. periods C and D), will be discussed. Also, the effect of time on stream (i.e. periods A and B compared with period E) will be touched upon.

#### 3.3.1. Estimation of $\alpha_{C_n}$ values

The weight fraction  $W_n$  of a hydrocarbon chain with  $n$  carbon atoms is defined by the ASF model as follows [46,47], assuming that each C-unit has the same weight:

$$W_n = n \cdot (1 - \alpha)^2 \cdot \alpha^{n-1} \quad (4)$$

where the propagation probability  $\alpha$  is independent of chain length. As a single  $\alpha$  value cannot explain the true product selectivity (the deviation is especially large in the C<sub>1</sub>–C<sub>5</sub> range), separate  $\alpha_{C_n}$  values

**Table 2**

Physicochemical properties, TOF in period A (after 10 h on stream) and  $S_{C_{5+}}$  in period B of the studied catalysts. IW: incipient wetness impregnation. ME: microemulsion. HT: hydrothermally treated.

Catalyst	Reduction temperature (K)	DOR, O <sub>2</sub> titr. (%)	DOR, TPR (%)	DOR used in calculations <sup>a</sup> (%)	Co dispersion (%)	Co particle size (from DOR + disp.) <sup>b</sup> (nm)	Co <sub>3</sub> O <sub>4</sub> cryst. size in calcined catalyst (XRD) (nm)	Co cryst. size (XRD) <sup>f</sup> (nm)	TOF after 10 h on stream <sup>d</sup> (s <sup>-1</sup> )	$S_{C_{5+}}$ in period B (%)
<i>γ</i> -Al <sub>2</sub> O <sub>3</sub>										
6Co (IW)	623	52	50	50	7.6	6	13	10	0.059	79.3
8Co (IW)	623	46	–	54	7.1	7	13	10	0.050	79.1
12Co (IW)	623	51	62	62	7.5	8	15	11	0.044	79.0
12Co + Re (IW)	623	63	92	92	9.7	9	16	12 [9]	0.066	80.3
12Co + Re (IW) HT	623	37	–	–	–	–	16	12	–	75.0
20Co (IW)	623	–	65	65	7.1	9	16	12	0.065	79.1
12Co + Re (ME)	673	22	67	67	5.0	13	amorph.	[amorph.]	0.026	69.1
12Co + 0.15B (IW)	623	48	56	56	7.4	7	14	11	0.059	82.1
12Co + Re (IW) Cl 573 K <sup>e</sup>	673	58	–	–	0.4	–	CoCl <sub>2</sub>	[25]	–	55.5
12Co + Re (IW) Cl 773 K	673	37	–	–	0.9	–	18	[16]	–	69.0
<i>α</i> -Al <sub>2</sub> O <sub>3</sub>										
4Co (IW)	623	–	98	98	7.5	13	29	22	0.044	85.7
6Co (IW)	623	–	–	98	5.2	18	34	26	0.044	84.8
12Co (IW)	623	–	99	99	4.3	22	26	20	0.049	84.0
12Co + Re (IW)	623	–	–	99	4.5	21	25	19	0.058	84.9
20Co (IW)	623	–	99	99	2.3	42	45	34	0.045	81.6
<i>α</i> -Al <sub>2</sub> O <sub>3</sub> (*)										
12Co + Re (IW)	623	67	–	99	3.5	27	44	33	0.071	86.5
12Co + Re (IW) HT	623	62	–	92	3.4	26	47	35	0.059	84.0
4.4Co + Re (ME)	673	61	–	90	7.3	12	14	11	0.050	77.4
4.4Co + Re (ME) HT	673	60	–	89	3.9	22	23	17	0.037	72.6
<i>α</i> -Al <sub>2</sub> O <sub>3</sub> (**)										
6Co (IW)	623	68	–	98	3.6	26	36	27	0.048	83.3
12Co (IW)	623	68	–	99	4.3	22	33	25	0.047	83.1
TiO <sub>2</sub>										
4Co (IW)	623	–	–	92	4.2	21	19	14	0.081	84.1
6Co (IW)	623	–	94	94	4.3	21	21	16	0.070	84.0
12Co (IW)	623	–	96	96	3.9	24	23	17	0.070	84.9
12Co + Re (IW)	623	–	96	96	4.7	20	19	14	0.092	87.2
12Co + Re (IW), RedOx	623	–	–	96	6.2 <sup>f</sup>	15	–	–	0.092	89.5
20Co (IW)	623	–	97	97	3.3	28	26	20	0.060	87.1
20Co (IW), less water	623	–	–	97	2.9	32	32	24	0.071	87.7
30Co (IW)	623	–	–	97	2.2	42	37	28	0.054	87.9
12Co + 0.044B (IW)	623	–	92	92	4.4	20	24	18	0.063	84.9
12Co + 0.15B (IW)	623	–	87	87	3.7	22	19	14	0.082	87.0
TiO <sub>2</sub> (*)										
6Co (IW)	623	60	–	94	3.3	28	19	14	0.107	86.0
12Co + Re (IW)	623	70	–	96	3.0	31	29	22	0.104	88.0
12Co + Re (ME)	673	64	89	89	5.5	16	13	10	0.136	84.9
TiO <sub>2</sub> (**)										
12Co (IW)	623	71	–	96	4.0	23	24	18	0.074	84.2
12Co + 0.15B (IW)	623	61	–	87	2.9	29	21	16	0.068	89.5

<sup>a</sup> DOR from TPR of reduced catalysts where data available. Otherwise estimated from inter-/extrapolations of available DOR (from TPR) data, or by comparison of DOR (from O<sub>2</sub> titr.) data and "translation" to DOR (from TPR).

<sup>b</sup> According to Eq. (1).

<sup>c</sup> Estimated from XRD of calcined samples according to Eq. (2). Bracketed values indicate XRD of reduced and passivated samples.

<sup>d</sup> Turnover frequencies (TOFs) calculated from gas flow rates and CO conversions in period A and from Co dispersion data.

<sup>e</sup> This catalyst was composed of CoCl<sub>2</sub> in its calcined state, which was accounted for when calculating DOR and Co dispersion.

<sup>f</sup> Calculated by assuming the same TOF as the corresponding catalyst without RedOx treatment.

for  $n = 1-6$  ( $\alpha_{C_1}-\alpha_{C_6}$ ) have been calculated in the present paper, each indicating the probability of chain growth of the  $C_n$  surface species. In order to calculate these individual  $\alpha_{C_n}$  values, the same approach as described by Bertole et al. [48] has been used. The expressions utilised are as follows [2]:

$$\alpha_{C_n} = \frac{r_{g,n}}{r_{g,n} + r_{t,n}} = \frac{\sum_{m=n+1}^{\infty} r_{Cm}}{\sum_{m=n+1}^{\infty} r_{Cm} + r_{Cn}} \quad (5)$$

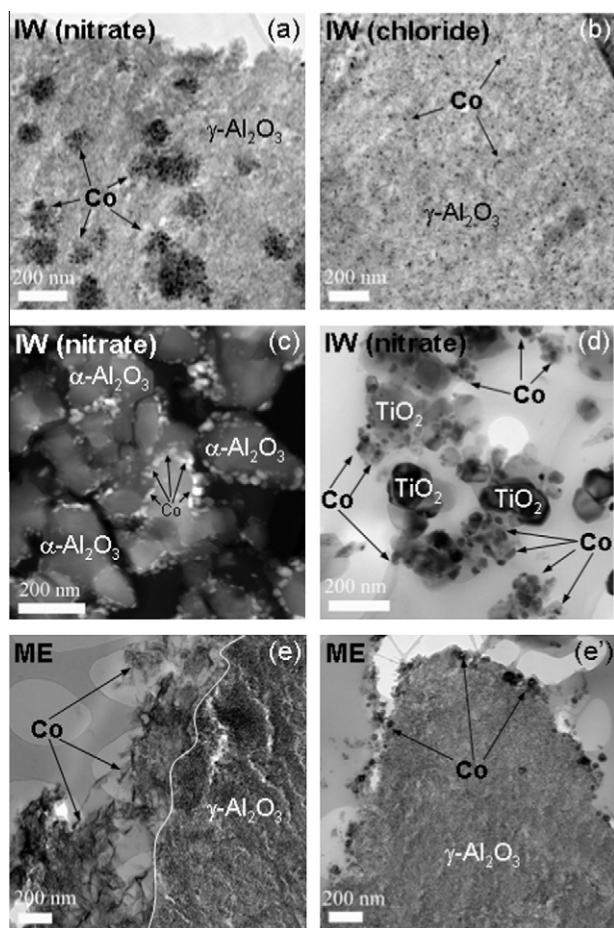
where  $r$  indicate molar rates, and subscripts  $g$  and  $t$  growth and termination, respectively. Since only a fraction of the total HC product was quantified ( $C_1-C_6$ ), it is necessary to make an assumption about the carbon-number distribution of the  $C_{7+}$  fraction in order to estimate the molar rates for the same fraction. The  $C_{7+}$  fraction is as-

sumed to follow an ASF distribution with the  $\alpha$  value that would give the same  $S_{C_{7+}}$  as the catalyst in question.

### 3.3.2. Results at reference case process conditions

The  $S_{C_{5+}}$  values in period B for all studied catalysts are given in Table 2. It can be seen that, in general, TiO<sub>2</sub>-supported catalysts have the highest  $S_{C_{5+}}$ , and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-supported catalysts the lowest. The ME-TiO<sub>2</sub>(\*) catalyst has a similar Co particle size as IW- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (12 wt% Co, 0.5 wt% Re) but a significantly higher  $S_{C_{5+}}$ , indicating that a possible Co particle size effect (above 6 nm) is subordinate to the effect of support material. Studying the TiO<sub>2</sub>-supported IW catalysts more closely suggests that the  $S_{C_{5+}}$  is increasing with Co particle size, while the opposite is true for the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>-supported IW catalysts. That TiO<sub>x</sub> decoration of Co particles reduces the  $S_{C_{5+}}$

has been reported previously [28,49], and the  $\text{TiO}_x$  decoration should reasonably be more severe the smaller the Co particles

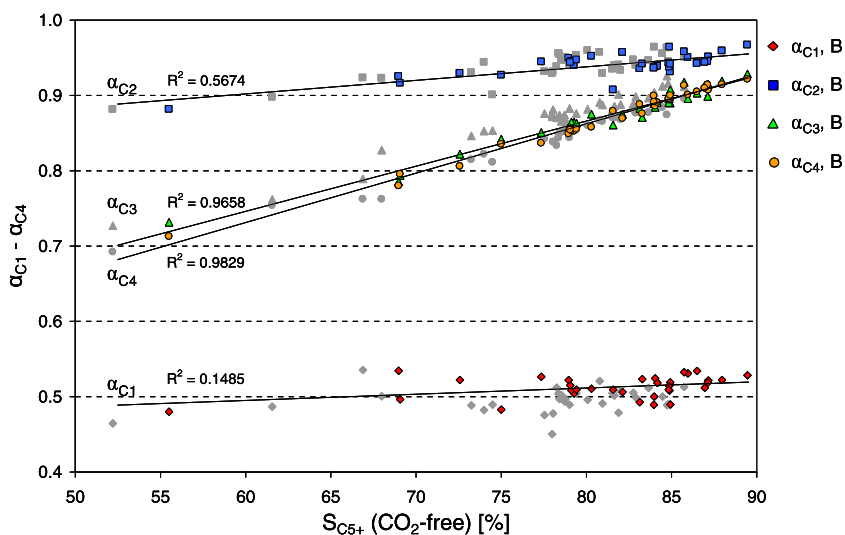


**Fig. 3.** TEM images of cross-sections of fresh IW- $\gamma\text{-Al}_2\text{O}_3$  (12 wt% Co, 0.5 wt% Re) catalysts prepared from Co nitrate (a) and Co chloride (b), fresh IW- $\alpha\text{-Al}_2\text{O}_3$  (12 wt% Co, 0.5 wt% Re) (STEM) (c), fresh IW- $\text{TiO}_2$  (12 wt% Co, 0.5 wt% Re) (d), fresh ME- $\gamma\text{-Al}_2\text{O}_3$  (~12 wt% Co) (e), and used ME- $\gamma\text{-Al}_2\text{O}_3$  (e'). The white line in (e) indicates the  $\gamma\text{-Al}_2\text{O}_3$  pellet boundary. The IW-catalyst prepared from  $\text{CoCl}_2$  (b) was calcined at 773 K.

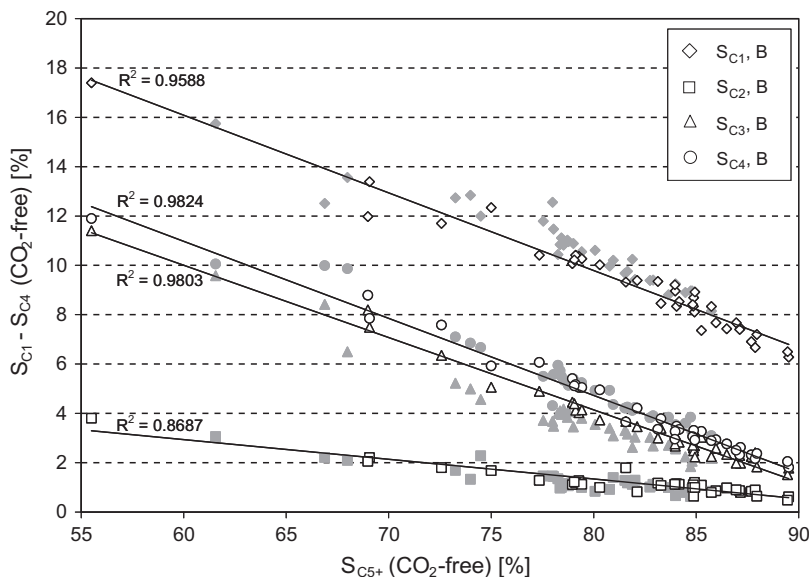
[50]. Also, a negative correlation between Co particle size and  $S_{\text{C}_{5+}}$  for  $\alpha\text{-Al}_2\text{O}_3$ -supported catalysts has been shown [20]. The RedOx treatment of IW- $\text{TiO}_2$  (12 wt% Co, 0.5 wt% Re) improves the  $S_{\text{C}_{5+}}$  significantly, although the Co particle size is apparently reduced. Possibly, the break-up of Co or  $\text{Co}_3\text{O}_4$  crystallites into smaller particles is connected with this increase in  $S_{\text{C}_{5+}}$ , which has been suggested earlier [19] for  $\gamma\text{-Al}_2\text{O}_3$ -supported catalysts. In fact, this “break-up” theory could also explain why smaller Co particles give higher  $S_{\text{C}_{5+}}$  for  $\alpha\text{-Al}_2\text{O}_3$ -supported IW catalysts, the catalyst with smaller Co particles having the largest  $d(\text{Co}_3\text{O}_4)/d\text{Co}^0$  ratio as estimated from XRD of calcined catalyst and from dispersion and DOR measurements of reduced catalyst. As already well known, both Re and B enhance  $S_{\text{C}_{5+}}$  [32,42]. The exceptional increase in  $S_{\text{C}_{5+}}$  when adding 0.15 wt% B to the IW- $\text{TiO}_2$ (\*\*) (12 wt% Co) can be ascribed to the simultaneous increase in Co particle size as estimated from dispersion and DOR measurements.

The catalysts presented in Table 2 provide selectivity data over a large range ( $S_{\text{C}_{5+}}$  in period B: 55.5–89.5%). It is therefore the primary focus of the present paper to discuss possible correlations between the selectivities and, in particular, to investigate the possible importance of secondary reactions and separate methanation sites on the  $S_{\text{C}_{5+}}$ . Fig. 4 shows the resulting individual  $\alpha_{\text{C}_n}$  values for  $n = 1-4$  vs.  $S_{\text{C}_{5+}}$ , and Fig. 5 shows the selectivities of  $\text{C}_1\text{-C}_4$  vs.  $S_{\text{C}_{5+}}$ , for the catalysts in periods A and B. Note that  $\alpha_{\text{C}_1}$ , defined by Eq. (5) above, has a different meaning from  $\alpha_1$  described in the introduction. Regression lines, calculated by using the method of least squares, are based on data obtained in period B. The goodness of fit for each regression line is represented by the indicated  $R^2$  value. It is striking how well the  $\alpha_{\text{C}_n}$  values, as well as the selectivities, fit to linear correlations irrespective of support material, Co loading, addition of promoters, preparation technique, Co particle size, degree of reduction and presence of a catalyst poison (CI). Furthermore, the conversion level does not seem to affect the interdependencies appreciably.

The lower  $R^2$  values of the regression lines of  $\alpha_{\text{C}_2}$  and  $S_{\text{C}_2}$  are partly explained by a higher relative standard deviation of the  $S_{\text{C}_2}$  (~6%) when compared to the  $S_{\text{C}_1}$  (~4%) and the  $S_{\text{C}_3}$  and  $S_{\text{C}_4}$  (~2% each), as estimated from multiple runs with the same catalyst. This is in turn explained by the very low concentration of  $\text{C}_2$  products in the effluent gas. Also, the small variation in  $\alpha_{\text{C}_2}$  values around the population average, i.e. the small slope of this regression line, contributes to the lower  $R^2$  value. The higher relative



**Fig. 4.**  $\alpha_{\text{C}_n}$  values ( $n = 1-4$ ) vs.  $S_{\text{C}_{5+}}$  for all catalysts in period A (grey symbols) and B (coloured symbols). CO conversion in period A is different for each catalyst varying between 3.5% and 30%. CO conversion in period B is ~40%. Experimental conditions: 483 K, 20 bar,  $\text{H}_2/\text{CO} = 2.1$ , pellet size 53–90  $\mu\text{m}$ . Regression lines are based on data points obtained in period B.



**Fig. 5.**  $S_{C1}$ – $S_{C4}$  vs.  $S_{C5+}$  for all catalysts in period A (grey, filled symbols) and B (open symbols). Experimental conditions as in Fig. 4. Regression lines are based on data points obtained in period B.

standard deviation for  $S_{C1}$  when compared to those of  $S_{C3}$  and  $S_{C4}$  probably stems from that  $S_{C1}$  is more sensitive to small changes in certain process parameters (e.g. temperature,  $H_2/CO$  ratio, partial pressure of water), which is discussed in Section 3.3.4. The  $\alpha_{C1}$  has the narrowest range of values (0.48–0.53 in period B) of all estimated  $\alpha_{Cn}$  values and, apparently, this small variation in the  $\alpha_{C1}$  data points is not well correlated with the  $S_{C5+}$ , as seen from the very low  $R^2$  value of this regression line (see Fig. 4).

It might be argued that the observed trends shown in Fig. 5 are partly a result of mathematics as the  $S_{C5+}$  is a function of the sum of the lower selectivities (see Eq. (3)). However, also  $S_{C5}$  and  $S_{C6}$  are linearly correlated with  $S_{C5+}$  (not shown), despite their higher relative standard deviations ( $S_{C5}$ :  $\sim 3\%$ ,  $S_{C6}$ :  $\sim 4\%$ ) and their mathematical independence of  $S_{C5+}$ , which confirms that individual HC selectivities are indeed well correlated with  $S_{C5+}$  (at least for the low carbon numbers investigated here).  $\alpha_{C5}$  and  $\alpha_{C6}$  were found to be nearly identical with  $\alpha_{C4}$ , which in turn is very close to  $\alpha_{C3}$ , as evidenced from Fig. 4.

One of the catalysts with the poorest  $S_{C5+}$  (61.6% in period A and 69.1% in period B, see Table 2) is the amorphous (with respect to cobalt)  $ME-\gamma-Al_2O_3$ , which is not surprising as Co particles smaller than approximately 6–8 nm are known to give low  $S_{C5+}$  [20,22,23]. What is interesting is that this catalyst, despite the obvious differences between this and the other catalysts (i.e. non-crystallinity, Co particles located mainly on external surface of support pellet), still falls relatively well on the experimental curves of Figs. 4 and 5. The much shorter diffusion distance for the  $ME-\gamma-Al_2O_3$  catalyst, compared to the other catalysts that have the Co particles inside the pores of their 53–90  $\mu m$  pellets, should imply a much lower probability of  $\alpha$ -olefin readsorption. This fact, apparently, does not result in a deviation from the trends shown in Figs. 4 and 5.

The catalyst with the absolutely poorest  $S_{C5+}$  (52.2% in period A and 55.5% in period B, see Table 2) is the  $IW-\gamma-Al_2O_3$  catalyst (12 wt% Co, 0.5 wt% Re) prepared from  $CoCl_2$  and calcined at 573 K, which is not surprising either as Cl is a known poison to Co-based FT catalysts [51]. The difference in Co particle size when compared to the corresponding catalyst prepared from  $Co(NO_3)_2$  (see Table 2) could of course also affect the selectivity, as could the different morphologies. The important issue in the current study is that the selectivities of a catalyst clearly under the influence of a poison follow the same trends as observed for non-poi-

soned catalysts. Furthermore, different morphologies of the catalysts, apparently, do not affect the interdependencies between the selectivities/ $\alpha_{Cn}$  values.

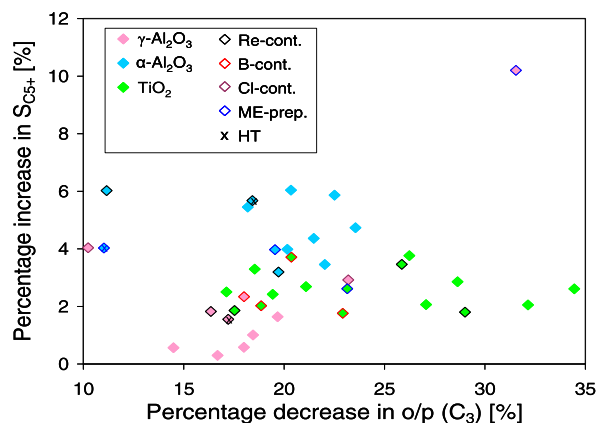
Puskas et al. [14] reported that the  $C_2$ – $C_4$  products obtained over supported Co catalysts were nearly constant fractions of the values expected from the corresponding ASF distributions (calculated from the  $\alpha$  value based on the  $C_6$ – $C_{10}$  products), depending little on the experimental conditions. This is essentially in agreement with the observations in the present study, with the difference that we have also found that there is a correlation between the  $C_1$  product and the estimated  $\alpha_{Cn}$  values (i.e.  $\alpha_{C2}$ – $\alpha_{C6}$ ) at fixed process conditions. Also, Mims and Bertole [24] have reported on a correlation between  $S_{C1}$  and a “ $\alpha$  value” estimated from the  $S_{C5+}/S_{C4}$  ratio, and Iglesia et al. [52] found a constant termination probability of  $C_1^*$  (and hence a constant  $\alpha_{C1}$ ) for a range of different Co catalysts at conditions similar to the reference case process conditions in the present paper. However, these studies were based on relatively narrow ranges of  $S_{C5+}$  values.

### 3.3.3. Olefin/paraffin ratios

A reduced space velocity (i.e. increased *bed* residence time) increases the extent of readsorption mainly of short  $\alpha$ -olefins [1], and the accompanying increase in  $S_{C5+}$  has been attributed to this readsorption (followed by chain growth) [2]. In Fig. 6, the percentage increase in  $S_{C5+}$  vs. the percentage decrease in  $C_3$  o/p (olefin/paraffin) ratio upon a halving of the space velocity has been plotted for all catalysts. The high values of the  $ME-\gamma-Al_2O_3$  catalyst are due to the crystallisation of the amorphous Co phase upon an increased partial pressure of water, as seen in Fig. 3e'. There are no correlations, neither overall nor within the same support. Similar “gunshot” plots were also obtained for the other measured o/p ratios (i.e. for  $C_2$ ,  $C_4$  and  $C_5$ ) and indicate that readsorption of short  $\alpha$ -olefins most probably cannot account for the increase in  $S_{C5+}$  upon a reduced space velocity. As higher  $\alpha$ -olefins are not appreciably affected by bed residence time [5,8], it may be concluded that differences in  $\alpha$ -olefin readsorption in general can only have a minor impact on the change in  $S_{C5+}$  upon changes in the space velocity.

The effect, if any, of  $\alpha$ -olefin readsorption on  $S_{C5+}$  in general, e.g. for different catalysts at similar conversion levels, is discussed in Section 4.2.1.





**Fig. 6.** Percentage increase in  $S_{C5+}$  vs. percentage decrease in  $C_3$  olefin/paraffin (o/p) ratio upon halving of the space velocity. Calculations based on selectivity and space velocity data from periods A and B. Experimental conditions as in Fig. 4. ME: microemulsion. HT: hydrothermally treated.

### 3.3.4. Changing process conditions

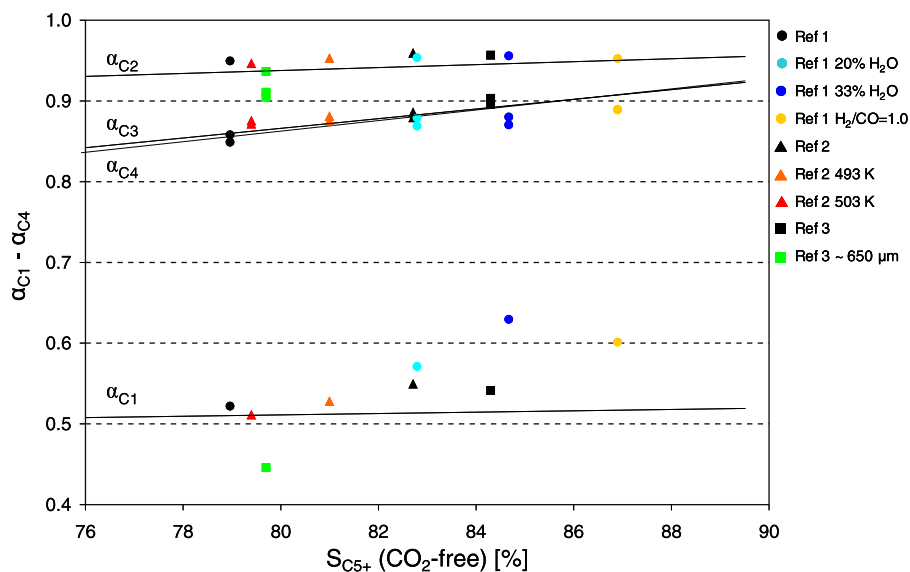
**3.3.4.1. General observations.** Changing the process conditions (e.g. temperature,  $H_2/CO$  ratio, catalyst pellet size, addition of water vapour, etc.) changes the  $\alpha_{Cn}$  values and selectivities. Fig. 7 shows the resulting changes in  $\alpha_{C1}-\alpha_{C4}$  upon some variations in process conditions for three catalysts (Refs 1–3, see caption of Fig. 7). It should be mentioned that the  $\alpha_{Cn}$  values for Refs 2 and 3 have been estimated by assuming ASF distribution of the  $C_{5+}$  fraction, since  $C_5$  and  $C_6$  data were missing. This gives slightly higher  $\alpha_{C1}$  values but does not affect the other  $\alpha_{Cn}$  values appreciably. Both the largest absolute changes and the largest deviations from the regression lines obtained under the reference case process conditions lie in the  $\alpha_{C1}$ . A higher sensitivity of  $\alpha_{C1}$  to changes in partial pressures of  $H_2$  and  $CO$  (keeping one of them constant), as well as a lower temperature dependence of  $\alpha_{C3}$  and  $\alpha_{C4}$  when compared to the other  $\alpha_{Cn}$  values, has been reported earlier [21,48]. It has also been reported that the increase in  $S_{C5+}$  upon water addition to Co-based catalysts mainly is coupled with a decrease in  $S_{C1}$  [29,32], which is in agreement with a relatively large increase in  $\alpha_{C1}$ . It should be mentioned that the synthesis gas conversion level was kept con-

stant upon changes in temperature, pellet size [21] and  $H_2/CO$  ratio by adjustment of the flow of synthesis gas. In case of water addition, however, no adjustment of synthesis gas flow was made. The conversion level of Ref 1 dropped from 40% to 30% and 20%, by introducing 20% and 33% water vapour, respectively, into the feed gas.

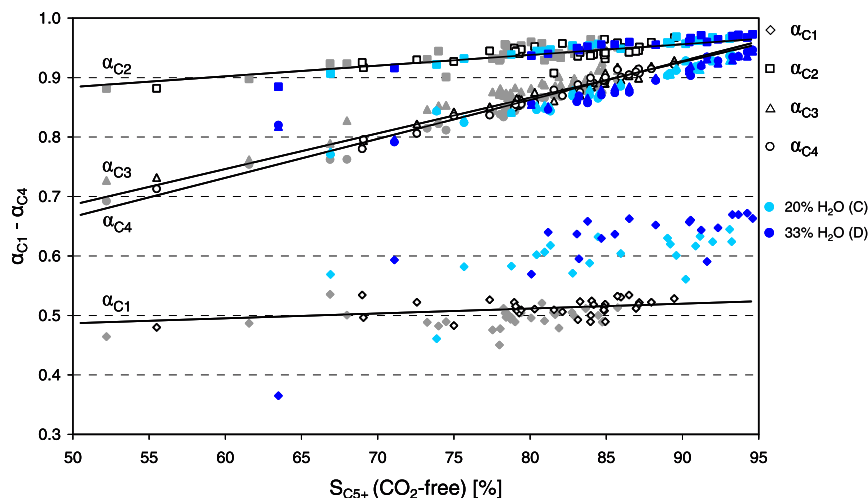
**3.3.4.2. Effect of water partial pressure.** The effect of external water addition on the  $\alpha_{Cn}$  values was investigated in more detail, and the results are illustrated in Fig. 8. New sets of trend lines form for the two different process conditions (20% and 33% water vapour added to the feed, respectively). Part of the overall larger variance in the  $\alpha_{C1}$  data upon external water addition, when compared to dry conditions, could be explained by a slightly less accurate temperature control and differences in conversion levels (i.e. partial pressures of water), as each catalyst responds individually with respect to the FT rate upon the addition of water (see Fig. 1) [53]. Furthermore, under the influence of added water vapour, a few data points clearly deviating from the linear relationships are appearing. Those are commented on in Section 3.3.5.

In general, the added water increases the  $S_{C5+}$  and, as mentioned above, the largest differences within the studied  $\alpha_{Cn}$  values lie in the  $\alpha_{C1}$  data, which increase with the amount of added water vapour. The  $\alpha_{C3}$  and  $\alpha_{C4}$  data points are gathered slightly below their respective regression lines obtained from period B. In Fig. 9, the  $S_{C1}$  and  $S_{C2-C4}$  vs.  $S_{C5+}$  are shown for periods A–D from which it may be seen that a catalyst system having a certain  $S_{C5+}$  at dry conditions (period A or B) in general has a significantly higher  $S_{C1}$  and somewhat lower  $S_{C2-C4}$  compared to a catalyst system that has the same  $S_{C5+}$  under the influence of water vapour in the feed. The “reaction pathways” for two selected catalysts going through periods A–D are also illustrated. It should be noted that the addition of water vapour to the feed does not change the slope of the selectivity regression lines.

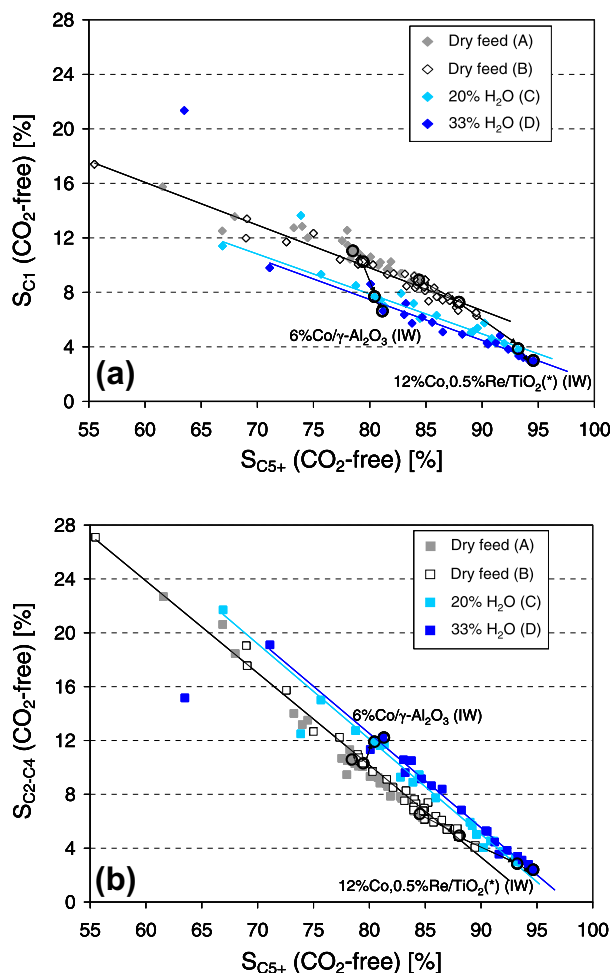
Fig. 10 shows the change in  $\alpha_{C1}$ ,  $\alpha_{C3}$  and  $\alpha_{C4}$  with the average  $P_{H_2O}/P_{H_2}$  in the reactor for some selected catalysts (excluding the clearly deviating catalysts discussed in Section 3.3.5). The  $\alpha_{C1}$  data points for all these catalysts fall, more or less, into one single curve, while the changes in the higher  $\alpha_{Cn}$  values are catalyst specific. It should be mentioned that, in general, no overall effect of Co particle size on the magnitude of the increase in  $S_{C5+}$ , either upon a



**Fig. 7.** Effects of changes in process conditions on the  $\alpha_{Cn}$  values for three catalysts. The lines are the regression lines from Fig. 4. Reference case conditions: 483 K, 20 bar, inlet  $H_2/CO = 2.1$ , pellet size 53–90  $\mu m$ . ● Ref 1 = 12 wt% Co/ $\gamma$ - $Al_2O_3$ . ▲ Ref 2 = 12 wt% Co/ $\gamma$ - $Al_2O_3$  (another batch of catalyst). ■ Ref 3 = 20 wt% Co, 0.5 wt% Re/ $\gamma$ - $Al_2O_3$  (from [21]). The “X%  $H_2O$ ” indicates that X% of the feed consisted of water vapour.



**Fig. 8.** Effect of external water addition (20% and 33%, respectively) on the  $\alpha_{Cn}$  values ( $n = 1-4$ ) vs.  $S_{C5+}$  for all catalysts. Grey, filled symbols indicate period A, open symbols period B and coloured symbols period C and D. Regression lines are based on data points obtained in period B.



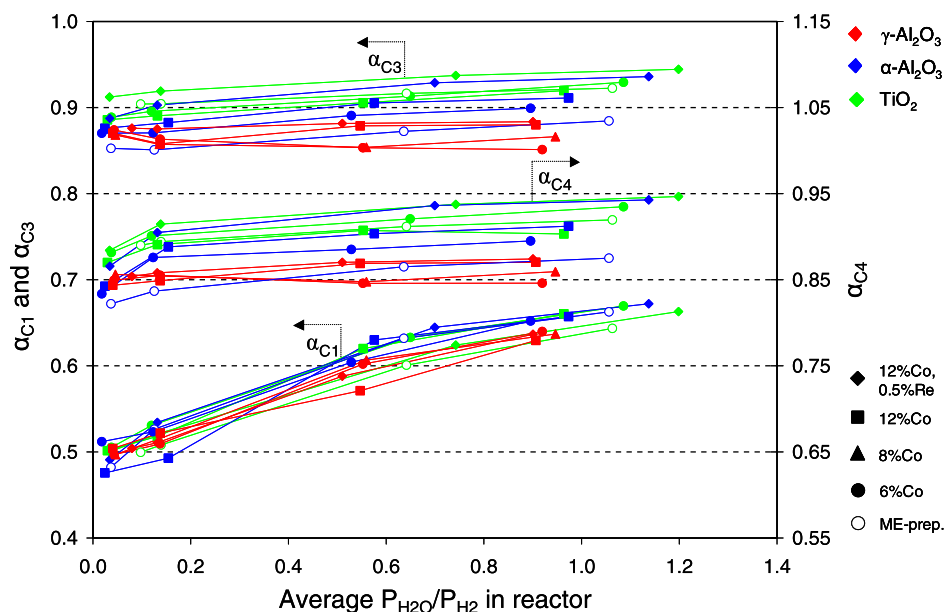
**Fig. 9.**  $S_{C1}$  (a) and  $S_{C2-C4}$  (b) vs.  $S_{C5+}$  for all catalysts in periods A–D. Regression lines are based on data points obtained in periods B, C and D, respectively, excluding the clearly deviating points in periods C and D. “Reaction pathways” through periods A–D for two catalyst examples are illustrated.

reduction in space velocity (A to B) or upon external addition of water, has been found. However, there is a clear effect of the support material. Typical for the wide-pore-supported catalysts (i.e.

TiO<sub>2</sub> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>) in this study is a large increase in  $S_{C5+}$  upon a lowered space velocity (see Fig. 6) and also a large increase in  $S_{C5+}$  upon external water addition. This can be understood from the increasing  $\alpha_{C1}-\alpha_{C4}$  values (see Fig. 10) going through periods A–D and is illustrated for 12%Co, 0.5%Re/TiO<sub>2</sub>(\*) (IW) in Fig. 9. Typical for the narrow-pore-supported catalysts (i.e.  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>) is a much smaller increase in  $S_{C5+}$  with a reduced space velocity and, especially for the catalysts with low Co loadings (i.e. 6 and 8 wt%), the increase in  $S_{C5+}$  upon external water addition is very small. Actually, the  $\alpha_{C2}-\alpha_{C4}$  values for the 6%Co/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (IW) catalyst decrease somewhat upon external addition of water vapour (see Fig. 10), which means that although  $S_{C5+}$  is slightly increased, so are the  $S_{C2}$ ,  $S_{C3}$  and  $S_{C4}$  (see Fig. 9). According to the sparse full product analysis data in the literature,  $\alpha_{\infty}$  was found to increase when adding water vapour to a Co/Ru/ZrO<sub>2</sub>/SiO<sub>2</sub> catalyst [29] and an unsupported Co catalyst [30]. The results in the present study, however, indicate a possibility of water addition to reduce the higher  $\alpha_{Cn}$  values, and possibly  $\alpha_{\infty}$ , although  $S_{C5+}$  is increased. This could, for instance, result in a lowered  $S_{C10+}$ , which is not desirable if wax is the product aimed for. In fact, the  $S_{C7+}$  for the 6%Co/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (IW) catalyst decreases from 69.5% in period B to 67.7% in period C, while the  $S_{C5+}$  increases from 79.4% to 80.4%.

**3.3.4.3. Effect of H<sub>2</sub>/CO ratio.** In Fig. 11a and b, the  $S_{C1}$  and  $S_{C2-C4}$  vs.  $S_{C5+}$  are shown, respectively, for inlet H<sub>2</sub>/CO ratios of 2.1 and 1.0. The CO conversion level ranged between 6 and 29% in the experiments with inlet H<sub>2</sub>/CO ratios of 1.0, which resulted in reactor-average H<sub>2</sub>/CO ratios between 0.8 and 0.97. The lower inlet H<sub>2</sub>/CO ratio was only tested for a small proportion of the catalysts, but still there is a clear difference in the selectivity correlations when compared to the higher inlet H<sub>2</sub>/CO ratio. Within the studied  $S_{C5+}$  range, a catalyst system having a certain  $S_{C5+}$  at inlet H<sub>2</sub>/CO = 2.1 in general has a higher  $S_{C1}$ , and somewhat lower  $S_{C2-C4}$ , compared to a catalyst system that has the same  $S_{C5+}$  at inlet H<sub>2</sub>/CO = 1.0. As opposed to the effect of water addition to the feed, the change in H<sub>2</sub>/CO ratio changes the slopes of the selectivity regression lines. In Fig. 11c, the  $\alpha_{C1}-\alpha_{C4}$  values vs.  $S_{C5+}$  for inlet H<sub>2</sub>/CO = 1.0 are shown, and it is obvious that  $\alpha_{C1}$  at these conditions is not invariant with  $S_{C5+}$ . It should be mentioned that this observation is not an effect of the small difference in reactor-average H<sub>2</sub>/CO ratio.

An example of the effect of lowering the inlet H<sub>2</sub>/CO ratio from 2.1 to 1.0 on the selectivity/ $\alpha_{Cn}$  values of a single catalyst was given



**Fig. 10.**  $\alpha_{C1}$ ,  $\alpha_{C3}$  and  $\alpha_{C4}$  vs. reactor-average  $P_{H_2O}/P_{H_2}$  ratio for selected catalysts. The four  $P_{H_2O}/P_{H_2}$  ratios for each catalyst are obtained from periods A, B, C and D, respectively.

in Fig. 7 and, obviously, the largest difference lies in the increase of  $\alpha_{C1}$  but also an increase in the higher  $\alpha_{Cn}$  values may be anticipated, as already reported in the literature [7,48].

### 3.3.5. Effect of time on stream on selectivity

The majority of the data points from period E, i.e. after five days on stream, still follow the regression lines obtained from period B relatively well. However, for four of the used catalysts, the selectivities/ $\alpha_{Cn}$  values deviate significantly from these correlations. The deviating catalysts are the hydrothermally treated 12%Co, 0.5%Re/ $\gamma$ - $Al_2O_3$  (IW), the one of the two 12%Co, 0.5%Re/ $\alpha$ - $Al_2O_3$  (IW) catalysts with the smallest Co particles (21 compared to 27 nm, or 19 compared to 33 nm if estimated from XRD of calcined catalyst), the ME- $\gamma$ - $Al_2O_3$  and the 12%Co, 0.5%Re/ $\gamma$ - $Al_2O_3$  (IW) prepared from  $CoCl_2$  and calcined at 773 K. The two significantly deviating points in period C and D (see Figs. 8 and 9) are for the hydrothermally treated 12%Co, 0.5%Re/ $\gamma$ - $Al_2O_3$  (IW). Fig. 12 shows the  $S_{C1}$  and  $S_{C2-C4}$  vs.  $S_{C5+}$  in periods B and E, and the deviation of the four catalysts implies that the  $S_{C1}$  is increased and the  $S_{C2-C4}$  is decreased for a certain  $S_{C5+}$ , when compared to the relationships established from period B. Table 3 shows the effect of time on stream on the deviation from the “ $S_{C1}/S_{C2-C4}$  vs.  $S_{C5+}$ ” relationship established from the regression lines in period B (Fig. 5) for all catalysts that were exposed to external water addition. The deviations in period B from this relationship were in the range of  $\pm 20\%$  (indicative of the variance in the data from which the relationship is established) while broadening to between  $-19\%$  and  $+183\%$  in period E due to the four significantly deviating catalysts. Common characteristics of these catalysts are a relatively large change (positive or negative) in  $S_{C5+}$ , comparing at similar conversion levels, going from period A–B to E, as well as a relatively high selectivity to  $CO_2$  in period E (see Table 3), although there are other catalysts showing the same level of  $S_{CO_2}$  without significant deviations.

From Table 3, it is evident that the main cause of the deviations is the large decrease in  $\alpha_{C1}$  for these four catalysts. The data in Table 3 also show that  $\alpha_{C1}$  is in most cases affected by time on stream independently of how the higher  $\alpha_{Cn}$  values are affected; for most catalysts,  $\alpha_{C1}$  is decreased from A–B to E, while the higher  $\alpha_{Cn}$  val-

ues have a larger tendency to increase somewhat. This suggests that the mechanism affecting  $\alpha_{C1}$  with time on stream is of a different nature than that affecting the higher  $\alpha_{Cn}$  values and, presumably, includes the formation of “pure methanation” sites.

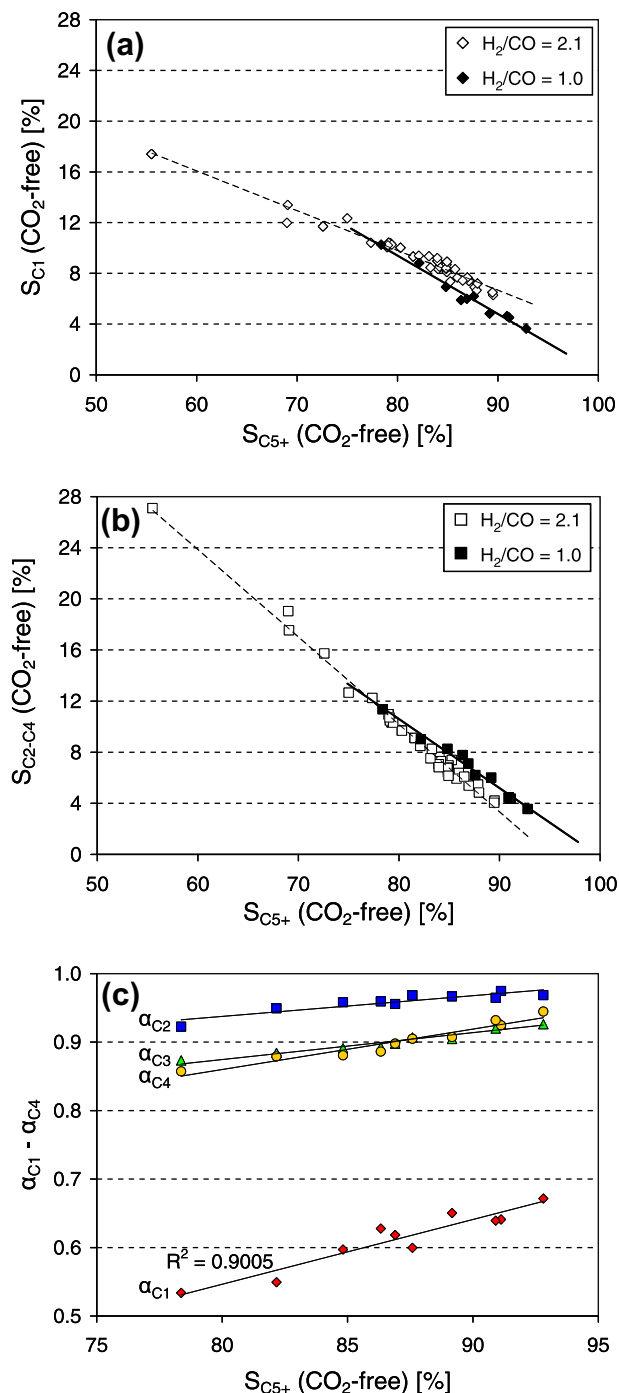
The ME- $\gamma$ - $Al_2O_3$  catalyst was re-reduced after the 5 days on stream, and it was possible to recover some of the losses in  $\alpha_{C1}$  (0.360  $\rightarrow$  0.424), which is in agreement with the presence of an oxidised cobalt phase. This phase may possibly be surface CoO, which has been reported to be active for  $CO_2$  formation [54]. The ME- $\gamma$ - $Al_2O_3$  catalyst also obtained as high  $\alpha_{C2}$ – $\alpha_{C4}$  values as the 12%Co/ $\gamma$ - $Al_2O_3$  (IW) catalyst, after having crystallised (see Fig. 3e') and after being re-reduced, which is another indication of that the diffusion distance range in the present study is not an important C-atom selectivity-governing parameter under the prevailing process conditions.

In general, as opposed to the  $TiO_2$  and  $\alpha$ - $Al_2O_3$ -supported catalysts, the IW-prepared  $\gamma$ - $Al_2O_3$  catalysts prepared from  $Co(NO_3)_2$  tended to reduce their  $S_{C5+}$  somewhat from period A–B to E (see Table 3), however, still following the selectivity regression lines obtained from period B relatively well. This difference lies mainly in the change of the higher  $\alpha_{Cn}$  values, and not in the  $\alpha_{C1}$  values. Hence, it may be concluded that the Co–Al compounds, reported to form with time on stream for  $\gamma$ - $Al_2O_3$ -supported catalysts [55–60], are not particularly active as “pure methanation” sites.

## 4. Discussion

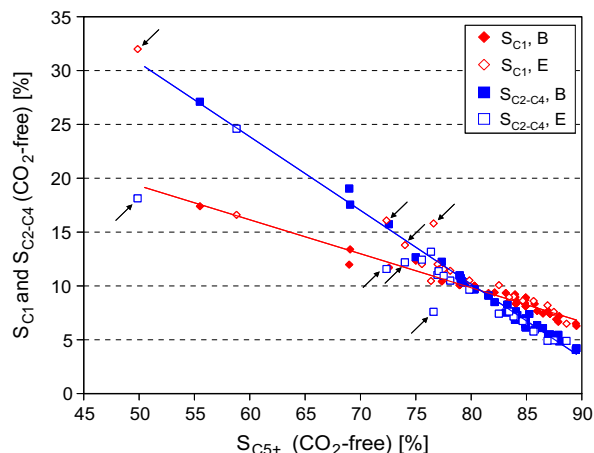
### 4.1. Validity of the estimated $\alpha_{Cn}$ values

By assuming a constant  $\alpha$  for  $n > 3$ , i.e.  $\alpha_{C5+} = \alpha_{C4}$ , the  $S_{C5+}$  was calculated based on the regression lines for  $\alpha_{C1}$ – $\alpha_{C4}$  in Fig. 4 and compared with the average measured selectivities (i.e. according to the regression lines in Fig. 5) obtained from the carbon mass balance over the reactor, within the experimental range (i.e.  $S_{C5+}$ : 50–90%). The relative error in the calculated  $S_{C5+}$  lies within  $\pm 1.5\%$ . This satisfactory match between calculated and measured selectivities, however, cannot be used to rule out the existence of two different  $\alpha$  values (i.e.  $\alpha_1$  and  $\alpha_\infty$ ) governing the distribution of the higher carbon-number HCs, since the  $\alpha_{Cn}$  estimations themselves are built



**Fig. 11.** (a)  $S_{C_1}$  vs.  $S_{C_{5+}}$  for inlet  $H_2/CO$  ratios 2.1 (period B) and 1.0. (b)  $S_{C_2-C_4}$  vs.  $S_{C_{5+}}$  for inlet  $H_2/CO$  ratios 2.1 (period B) and 1.0. (c)  $\alpha_{C_n}$  values ( $n = 1-4$ ) vs.  $S_{C_{5+}}$  for inlet  $H_2/CO = 1.0$ .

upon the assumption that the  $C_{7+}$  fraction has a constant  $\alpha$ . The observation that the  $\alpha_{C_4}-\alpha_{C_6}$  values are relatively constant for each catalyst, as mentioned in Section 3.3.2, is, however, not an effect of this assumption. Furthermore, the fact that there are clear relationships between the estimated  $\alpha_{C_1}-\alpha_{C_6}$  values and the  $S_{C_{5+}}$  at constant process conditions suggests that if two  $\alpha$  values describe the higher carbon-number product distribution, there should reasonably be a catalyst-property-independent correlation between them (for a constant conversion level). The change in  $\alpha$  value with carbon number ( $\alpha_1 \rightarrow \alpha_\infty$ ) would then logically be explained by a



**Fig. 12.** Illustration of four deviating catalysts: effect of time on stream (including exposure to high partial pressures of water) on the  $S_{C_1}$  and  $S_{C_2-C_4}$  vs.  $S_{C_{5+}}$ , with significantly deviating data points indicated by arrows. The regression lines are based on data points obtained in period B.

chain-length-dependent  $\alpha$ -olefin readsorption followed by further chain growth.

It has been reported that  $\alpha_\infty$  remains unchanged by changes in space velocity while, for instance,  $S_{C_{5+}}$  varies [5]. However, the positions of the " $\alpha_{C_n}$  vs.  $S_{C_{5+}}$ " regression lines in Fig. 4 are almost independent of conversion level (space velocity). The estimations of these lower  $\alpha_{C_n}$  values ( $\alpha_{C_1}-\alpha_{C_4}$ ) are less affected by the  $C_{7+}$  assumption and may therefore be considered more accurate and, probably, the correlations between the lower  $\alpha_{C_n}$  values and  $S_{C_{5+}}$  are indeed more or less independent of conversion level within the studied range.

## 4.2. Mechanistic considerations

### 4.2.1. Secondary reactions

In addition to the finding that there are no correlations between changes in  $S_{C_{5+}}$  and changes in o/p ratio upon halving of the space velocity (see Fig. 6), there are further observations indicating the minor effect of secondary reactions on  $S_{C_{5+}}$  in general. For instance, the relatively high  $\alpha_{C_2}$  also for the ME- $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst with minor diffusion distance suggests that the low  $S_{C_2}$  generally observed for Co-based catalysts, as discussed in the introduction, is not due to a high extent of  $C_2$  olefin readsorption but rather due to a particularly high reactivity of the  $C_2^*$  surface specie towards chain growth. Alternatively, if the diffusion distances prevailing in the present study are too short to affect the extent of secondary reactions, as it has been shown that  $\alpha$ -olefin readsorption takes place also with zero diffusion distance [8], the fact that we obtain different selectivities is in itself a proof of the minor effect of secondary reactions on  $S_{C_{5+}}$ .

Borg et al. [20] showed that there was no overall correlation between o/p ratio (for  $C_3$ ) and  $S_{C_{5+}}$  for Co-based catalysts. Correlations only existed within the same support material. The existence of catalyst-property-independent overall correlations between the individual HC selectivities ( $S_{C_1}-S_{C_6}$ ) and the  $S_{C_{5+}}$ , as shown in the present study, therefore, indicates that different mechanisms govern the production of the sum of the olefin and paraffin and the production of the separate olefin and paraffin (of a specific carbon number), at least for the low carbon numbers investigated in the present study. This, again, suggests that differences in  $\alpha$ -olefin readsorption can only have a minor effect on the  $S_{C_{5+}}$ , which is in agreement with Kuipers et al. [8] who found that the extent of readsorption with further chain growth of short  $\alpha$ -olefins was very small.



**Table 3**  
Effect of time on stream (including exposure to high partial pressures of water) on the deviation from predicted  $S_{C1}/S_{C2-C4}$  ratio, and on the  $\alpha_{Cn}$  values, for the catalysts exposed to external water addition. Changes in  $S_{C5+}$  and  $S_{C1}$  from period A–B to E, as well as  $S_{CO_2}$  in period E, are also included. The four clearly deviating catalysts in period E are marked with \*.  
IW: incipient wetness impregnation. ME: microemulsion. HT: hydrothermally treated.

Catalyst	Percentage deviation in $S_{C1}/S_{C2-C4}$ ratio from model <sup>a</sup> , period B (%)	Percentage deviation in $S_{C1}/S_{C2-C4}$ ratio from model <sup>a</sup> , period E (%)	Change in $S_{C5+}$ A–B to E <sup>b</sup> (units of %)	Change in $S_{C1}$ A–B to E <sup>b</sup> (units of %)	$S_{CO_2}$ in period E (%)	Percentage change in $\alpha_{Cn}$ value A–B to E <sup>c</sup> (%)		
						$\alpha_{C1}$	$\alpha_{C3}$	$\alpha_{C4}$
$\gamma\text{-Al}_2\text{O}_3$								
6Co (IW)	+6	+16	−1.9	+0.9	0.8	−1.9	−1.4	−0.7
8Co (IW)	+3	+19	−1.4	+1.0	0.8	−3.3	−0.3	−0.4
12Co (IW)	−1	+20	−0.4	+0.8	0.4	−4.0	0	+0.9
12Co + Re (IW)	+7	+25	−2.1	+1.3	0.6	−4.4	−0.3	−1.6
*12Co + Re (IW) HT	+17	+183	−23.9	+19.4	1.9	−42.9	−7.7	−5.8
*12Co + Re (ME)	+2	+87	+10.6	+0.8	1.1	−16.4	+11	+12.7
12Co + Re (IW) CI 573 K	−1	+2	+3.7	−1.0	1.2	+0.6	+2.5	+3.3
*12Co + Re (IW) CI 773 K	−16	+36	+7.1	+1.0	0.8	−16.0	+6.9	+9.1
$\alpha\text{-Al}_2\text{O}_3$								
*12Co + Re (IW)	+20	+140	−5.5	+5.7	1.2	−22.8	+0.4	+1.0
$\alpha\text{-Al}_2\text{O}_3(*)$								
12Co + Re (IW)	−9	+11	+0.7	−0.1	0.5	−0.5	−1.3	+3.1
12Co + Re (IW) HT	+18	+28	+0.3	−0.1	1.0	−0.2	+0.3	+0.3
4.4Co + Re (ME)	−4	+15	−0.9	+0.9	0.3	−3.6	+0.6	0
4.4Co + Re (ME) HT	−6	−8	+1.2	−0.2	0.6	−0.8	+2.6	−0.5
$\alpha\text{-Al}_2\text{O}_3(**)$								
6Co (IW)	−7	+14	−0.4	+0.8	1.3	−3.7	+0.2	+2.4
12Co (IW)	+14	+6	+3.4	−1.7	0.9	+6.3	+1.4	+3.0
$TiO_2$								
12Co + Re (IW)	−3	+5	+1.0	−0.2	0.4	−0.7	+1.1	+1.0
$TiO_2(*)$								
6Co (IW)	−7	−19	+2.3	−1.0	0.2	+3.1	+1.9	+1.7
12Co + Re (IW)	−3	+21	−0.2	+0.6	0.5	−4.2	+0.1	+1.5
12Co + Re (ME)	+12	+8	+0.9	−0.8	0.2	+3.9	−0.1	+0.2
$TiO_2(**)$								
12Co (IW)	+1	+18	+2.6	−0.5	0.5	−2.4	+1.9	+3.3

<sup>a</sup> The model value is the  $S_{C1}/S_{C2-C4}$  ratio obtained from the selectivity regression lines in Fig. 5 for the  $S_{C5+}$  of the catalyst in period B or E.

<sup>b</sup> The selectivity in period A–B is obtained from inter-/extrapolation of the selectivity values in periods A and B to the same conversion level as in period E.

<sup>c</sup> The  $\alpha_{Cn}$  values in period A–B are obtained from inter-/extrapolation of the  $\alpha_{Cn}$  values in periods A and B to the same conversion level as in period E.

The suggested correlation between  $\alpha_1$  and  $\alpha_\infty$  at constant process conditions (see Section 4.1) implies that, within the range of the studied catalyst variables, possible differences in *pore* residence time – a parameter mostly affecting readsorption of higher  $\alpha$ -olefins [5] – do not affect the selectivities ( $S_{C1}$ – $S_{C5+}$ ) or  $\alpha_{Cn}$  values appreciably. This has been confirmed earlier by Rytter et al. [21] who, through a detailed product analysis, found that  $\alpha_\infty$  was hardly changed upon an increase in catalyst pellet size from 50 to 650  $\mu\text{m}$ .

#### 4.2.2. Methane production vs. higher HC production

In the following subparagraphs, we present some tentative mechanistic models able to explain our main observations.

4.2.2.1. Possible mechanistic models. The key observations of the present study are as follows:

- linear correlations between selectivity to methane (and other light products) and  $S_{C5+}$  and
- a relatively constant  $\alpha_{C1}$  for a range of catalysts having widely different  $S_{C5+}$  selectivities investigated in a fixed-bed under standard low-temperature FT conditions.

As there are specific correlations between the  $S_{C1}$  and the other selectivities under all studied process conditions (see for instance Fig. 5), the methane production rate is intrinsically coupled to the production rate of higher HCs. This is in line with a common pool of precursors (here denoted  $\text{CH}_2^*$  and referred to as the *monomer*), as suggested previously from SSITKA (steady-state isotopic transient kinetic analysis) measurements [61–63]. The relatively constant site activity of the studied catalysts (see Table 2) indicates

further that the rate-determining step is the same irrespective of the length of the HC products and, hence, lies within the formation of the monomer, as proposed earlier by Mims and McCandlish [61] and van Dijk et al. [62,63]. A similar site activity for all the studied catalysts also indicates that the monomer formation takes place at a general Co surface present in all catalysts. In summary, the existence of separate methane-producing sites, as sometimes proposed to explain selectivity variations [6], may be ruled out for the (fresh) studied catalysts. However, as mentioned in Section 3.3.5, four of the catalysts apparently developed such “pure methanation” sites after exposure to high partial pressures of water.

Although there are several proposals for activation steps and intermediate surface species, we denote the key entities simply as  $\text{CH}_2^*$ ,  $\text{CH}_3^*$  and  $\text{H}^*$ , thus capturing the building blocks of the hydrocarbon chain. Methane formation and chain initiation are, hence, schematically illustrated as follows:



The chain-growth probability of  $\text{CH}_3^*$ ,  $\alpha_{C1}$ , may then be expressed as a function of surface coverages ( $\theta$ ) of the monomer  $\text{CH}_2^*$  and of  $\text{H}^*$ , and of rate constants ( $k$ ) to chain growth and termination of  $\text{CH}_3^*$  as shown below:

$$\alpha_{C1} = \frac{r_{C2+}}{r_{C2+} + r_{C1}} = \frac{k_{g,1} \cdot \theta_{\text{CH}_3^*} \cdot \theta_{\text{CH}_2^*}}{k_{g,1} \cdot \theta_{\text{CH}_3^*} \cdot \theta_{\text{CH}_2^*} + k_{t,1} \cdot \theta_{\text{CH}_3^*} \cdot \theta_{\text{H}^*}} = \frac{\theta_{\text{CH}_2^*}}{\theta_{\text{CH}_2^*} + \frac{k_{t,1}}{k_{g,1}} \cdot \theta_{\text{H}^*}} \quad (8)$$

For a constant  $\alpha_{C1}$  to occur according to Eq. (8), the surface coverages of  $\text{CH}_2^*$  and  $\text{H}^*$ , as well as the  $k_{t,1}/k_{g,1}$  ratio, need to be the same

for all the catalysts investigated. Relatively constant surface coverages (e.g.  $\theta_H$ ,  $\theta_{CH_x}$ ,  $\theta_{CO}$ , measured by SSITKA) irrespective of Co particle size (>6 nm), support material and HC selectivities have recently been reported in the literature [23,44,45]. The constant  $k_{t,1}/k_{g,1}$  ratio could reflect an intrinsic property of an active cobalt surface, i.e.  $k_{t,1}$  and  $k_{g,1}$  independent of chain-growth probability of the longer chains. This could be rationalised by a two-site model in which methane and (at least)  $C_2^*$  are formed at one type of site from the same  $CH_3^*$  pool, while further chain growth and termination of the  $C_{2+}$  chains (alternatively only termination) take place at a separate subgroup of sites present in low concentration. In this model, the formation of methane and  $C_{2(+)}$  would take place at the Co surface responsible for the monomer production, i.e. at the general Co surface sites present in all of the studied catalysts and the number of which are estimated from chemisorption measurements. The  $\alpha_{C_{2+}}$  values and, hence, the  $S_{C_{5+}}$  would depend on the ratio of the number and/or activity of the two types of sites.

An alternative explanation to the relatively constant  $k_{t,1}/k_{g,1}$  ratio is that it is a coincidence for the chosen process conditions and that both  $k_{t,1}$  and  $k_{g,1}$  vary (in the same direction) with the  $S_{C_{5+}}$  of the catalysts. Again, a two-site model is envisioned in which the monomer and methane are the only products from the general Co surface sites. The monomers not converted into methane then migrate to separate chain-growth sites (also capable of termination) present in low concentration, to form all possible products (including methane). Similar two-site models with migrating monomers have been proposed earlier [63,64]. An apparent constant overall  $\alpha_{C_1}$  at certain process conditions could be the result of the “extra” production of methane taking place at the general Co sites, whereas the  $\alpha_{C_n}$  values at the chain-growth sites are all increasing with the  $S_{C_{5+}}$  and governed by the ratio of the number and/or activity of the two types of sites. Supporting evidence for two routes responsible for methane production over Co-based FT catalysts can also be found in the literature [23,45,62,63,65].

**4.2.2.2. Further remarks on selectivity.** The results from the experiments with an inlet  $H_2/CO$  ratio of 1.0 indicate that  $\alpha_{C_1}$  is not invariant with  $S_{C_{5+}}$  for all process conditions. This is possible to explain with the model in which methane production takes place at two types of sites. With an inlet  $H_2/CO$  ratio of 2.1 (periods A and B), the lowest theoretical  $S_{C_1}$  approaches 5% (at  $S_{C_{5+}} = 95\%$ ), extrapolating the regression lines of Fig. 9 to  $S_{C_{2-C_4}} = 0\%$  (i.e.  $\alpha_{C_{2+}} = 1$ ). Similarly, we can estimate the lowest  $S_{C_1}$  upon addition of 20% and 33% water to the feed at 3% and 2%, respectively. Apparently, water inhibits the “extra” methane production at the general Co surface, which is further indicated by the similar change in  $\alpha_{C_1}$  with changes in the average  $P_{H_2O}/P_{H_2}$  for the studied catalysts. The general and unequivocal effect of water on the selectivity observed for all catalysts, hence, seems to be limited to this general Co surface.

When the inlet  $H_2/CO$  ratio is lowered to 1.0, there seems to be no “extra” production of methane, as both  $S_{C_1}$  and  $S_{C_{2-C_4}}$  approaches zero approximately at  $S_{C_{5+}} = 100\%$  (see Fig. 11a and b), which could explain why  $\alpha_{C_1}$  now is increasing with  $S_{C_{5+}}$  (see Fig. 11c). However, the effect of the  $H_2/CO$  ratio is believed to be related to both types of sites by means of changing the relative abundance of the monomer and of hydrogen on the total cobalt surface and thereby directly affecting, for instance, the termination rate at the subgroup sites. The difference in selectivity correlations when adding water and when reducing the inlet  $H_2/CO$  ratio, as seen from Figs. 9 and 11, suggests that the positive effect of water on  $S_{C_{5+}}$  is not directly linked to a lower surface coverage of hydrogen.

In addition to different extents of secondary reactions caused by differences in mass transfer limitations [2], local differences in availability of adsorbed hydrogen (e.g. due to differences in spill-

over capacity of the support materials or due to  $TiO_x$  decoration) [25,28] or monomeric carbon [24] have been proposed to explain the differences in  $S_{C_{5+}}$  among various Co-based catalysts (with Co particles >6 nm). Irrespective of the above proposed mechanistic models, the observation that the overall  $\alpha_{C_1}$  is more or less the same for all catalysts at the reference case process conditions, and with external water addition, indicates that the differences in  $S_{C_{5+}}$  between the catalysts in the present study, however, cannot be ascribed to differences in surface coverages at the general Co surface. However, varying availability of hydrogen and monomeric carbon at the Co/support interfacial perimeter (i.e. at non-general Co sites) cannot be excluded.

Finally, it should be commented that the interrelationships observed in the present study probably do not apply generally for catalysts with Co particles smaller than approximately 6 nm, as it was recently shown that such particles differ considerably in their surface coverages (e.g.  $\theta_H$ ,  $\theta_{CH_x}$ ,  $\theta_{CO}$ ) compared to larger Co particles [23].

## 5. Conclusions

In the range of the studied process conditions and catalyst variables, there is a specific interrelationship (for fixed process conditions) between the HC selectivities also for the non-ASF distributed part of the FT product spectrum (i.e.  $\sim C_1-C_5$ ) irrespective of the properties of the Co-based catalyst. Hence, there is a mechanistic link between the formation of methane and higher HCs, presumably a common precursor (monomer) pool, and the existence of “pure methanation” sites may, therefore, be ruled out for the (fresh) studied catalysts. It is noteworthy that  $\alpha_{C_1}$  is more or less constant for 36 catalysts exposing a large  $S_{C_{5+}}$  range, when investigated at standard low-temperature FT conditions ( $H_2/CO = 2.1$ ). This indicates that although resulting from a common pool of intermediates, the mechanism of methane formation differs from that of higher HCs. It seems, however, like the constant  $\alpha_{C_1}$  behaviour is not valid at other  $H_2/CO$  ratios.

For a small proportion of the studied catalysts, the exposure to high partial pressures of water seemingly involved changes in the surface composition, may be to  $CoO$ , resulting in the formation of “pure methanation” sites possibly responsible for a separate precursor pool. Surface Co–Al compounds reported to form in  $Co/\gamma-Al_2O_3$  catalysts with time on stream were, however, found not to be particularly active as “pure methanation” sites.

For the conditions studied, the reason for a high  $S_{C_{5+}}$  is found to be essentially a high intrinsic chain-growth probability and not a result of an enhanced  $\alpha$ -olefin readsorption. The increase in  $S_{C_{5+}}$  upon a reduction in space velocity is, therefore, at least partially believed to be due to the higher partial pressure of water as a result of an increased conversion level. The linear interdependencies between the propagation probabilities  $\alpha_{C_n}$  as a function of  $S_{C_{5+}}$  vary with process conditions; however,  $\alpha_{C_1}$  is in most cases significantly more affected than the other  $\alpha_{C_n}$  values. A lowered space velocity, as well as external water addition, increases the  $S_{C_{5+}}$  for essentially all catalysts. However, the individual response in  $\alpha_{C_{2-C_4}}$  values and selectivities upon water exposure varies greatly with catalyst and, seemingly, mostly with the choice of support material, while  $\alpha_{C_1}$  is affected in a similar way for all catalysts (except for the catalysts developing “pure methanation” sites). The general and unequivocal effect of water addition on the hydrocarbon selectivities is found to be limited to the decrease in  $S_{C_1}$ . Reducing the  $H_2/CO$  ratio also increases the  $S_{C_{5+}}$  but results in different selectivity interdependencies compared to when increasing the water partial pressure.

In the present study, careful quantitative analysis was only made of the  $C_1-C_4$  HC products. The data, therefore, do not provide evidence for a catalyst-property-independent correlation between

the lower HC selectivities and  $\alpha_{\infty}$  (at constant process conditions and conversion levels), although there are such indications.

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